

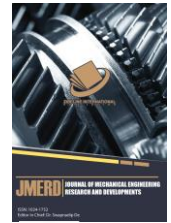


ZIBELINE INTERNATIONAL

ISSN: 1024-1752 (Print)

CODEN: JERDFO

Journal of Mechanical Engineering Research & Developments (JMERE)

DOI : <http://doi.org/10.26480/jmerd.01.2019.64.70>

RESEARCH ARTICLE

RESEARCH AND CALCULATION OF THE BIOGAS FUEL SUPPLY SYSTEM FOR A SMALL MARINE DIESEL ENGINE

Van Hai Nguyen*, Duc Thiep Cao, Thi Hien Do

Vietnam Maritime University, Haiphong city, Vietnam

*Corresponding Author Email: hainv.vck@vimaru.edu.vn

This is an open access article distributed under the Creative Commons Attribution License, which permits unrestricted use, distribution, and reproduction in any medium, provided the original work is properly cited

ARTICLE DETAILS

ABSTRACT

Article History:

Received 22 November 2018

Accepted 26 December 2018

Available online 27 January 2019

Biogas is a type of renewable energy generated from solar energy, so the combustion product of biogas will not emit CO₂ which affects the environment. Currently, the use of biogas for internal combustion engines such as vehicles and diesel generators is used in many countries in the world as well as in Vietnam. For the shipping industry, diesel engines are used, so the use of biogas on marine engines to meet the target of reducing harmful engine emissions into the environment and application strategies Renewable fuel sources for use on marine engines are very significant. The paper shows the results of the calculation of the conversion of diesel generators to become engines with biogas/diesel mixed fuel with the main contents: studying the necessary equipment for conversion engine to use biogas-diesel blended fuel.

KEYWORDS

Biogas, fuel supply system, research, and design for conversion of a diesel engine

1. INTRODUCTION

Energy issues in the world are currently being debated regarding technical, economic and environmental aspects [1]. Energy sources are being used today, such as coal, oil, natural gas and even nuclear energy will become exhausted [2]. Oil is the first source of fossil energy that we must mention [3]. The problems of this type of fuel such as reserves catches and prices are always a global theme [4]. Petroleum products, a form of fossil energy such as oil (DO, distillate fuel), or heavy fuel, also known as fuel oil (HFO), are traditional fuels used for ship engines [5]. Therefore, if there is no sooner to find an appropriate alternative energy source, the energy supply for the shipping industry in the coming time also faces a serious shortage [6,7].

If the combustion process of the air and fuel mixture in the combustion chamber of the engine is ideal, the combustion product is only CO₂, H₂O, N₂, and a small fraction of SO₂ [8-10]. However, due to the heterogeneity of the mixture of air and fuel as well as due to the complexity of the physiological phenomena that occur during combustion, the combustion product will have environmental pollutants [11,12]. In the toxic fire products of internal combustion engines, CO_x, HC, NO_x is the main factors causing environmental pollution, climate change, harm to human health [13-15].

CO₂ gas is the main factor causing an increase in the greenhouse effect due to fossil fuel combustion products increasing the temperature of the earth's surface [4,16]. When the temperature of the atmosphere increases, there will be a lot of special harms, such as sea level rise. Sea level rose to 0.2-0.4m when atmospheric temperature increased by 1°C. Vietnam is one of the countries considered to be severely affected by rising sea levels. Also, when the temperature of the earth's surface increases, phenomena such as desertification and barren land are rapidly causing great impacts

on the agricultural sector. NO_x, CO are toxic substances that harm human health [17].

The use of fossil fuels has seriously polluted the atmosphere. CO₂, the fossil fuel combustion product is a greenhouse gas, the main culprit that raises ground temperature leading to climate change and sea level rise, threatening the life of humanity. On the other hand, there are limited sources of fossil fuels [18]. High-intensity exploitation in recent decades has caused this energy source to deplete rapidly. The recent rise in oil prices reflects this situation. The ability to find a large source of oil that can be commercially exploited as in the past has almost no hope.

One question is when fossil fuels are exhausted, what energy sources will humans use instead [19]. Nuclear energy has long been considered salvation, but the Chernobyl nuclear disaster in 1986 and Fukushima in 2011 has caused people to re-issue the problem. Germany has declared a complete abandonment of nuclear energy by 2022; Japan is also considering closing nuclear plants after the double-earthquake-tsunami-nuclear disaster ... only a source of renewable energy Solar-based creation can guarantee the maintenance of human civilization until the solar system disappears.

Environmental protection is not only a requirement of each country but also a region that has a global meaning [20]. Depending on the conditions of each country, rules and standards on environmental pollution are applied at different times and severity levels [21].

Biogas is an abundant source of renewable energy in traditional agricultural countries like Vietnam [22,23]. Researching technology using

them is important in fossil fuel savings and reducing the level of greenhouse gas emissions in the atmosphere [24].

Biogas is renewable energy derived from solar energy, so using this energy does not increase the concentration of greenhouse gases in the atmosphere [25]. The presence of CO₂ in biogas reduces heating value, reduces the burning rate but it increases the anti-knocking properties of the fuel, allowing to increase the compression ratio of the engine [26,27]. So in cases where biogas is used at the production site, we do not need to filter out CO₂. This allows us to reduce the operating costs of the system providing biogas for the engine [28,29].

Biogas is the product of anaerobic decomposition of organic compounds. The composition of biogas is mainly CH₄, CO₂ and other components such as N₂, H₂S, O₂, CO, ... [30,31]. Methane is used as fuel and the main component of biogas and other components do not have the role of heat generation during combustion of biogas [28].

The conversion of traditional diesel engines to run on biogas can be done by the method of spark ignition engine, dual fuel (biogas-diesel) method [16,21]. Dual fuel method uses a minimum amount of diesel injection to ignite the ignition engine ignition [32]. In operation, the minimum amount of injection required for ignition only accounts for less than 10% of the injection when a diesel-powered engine is in rated mode [33,34]. However, to prevent the nozzle from overheating during operation with

biogas, the minimum amount of spraying should be maintained between 15% and 20% of diesel injection in the rated mode [35]. Biogas-diesel bi-fueled engine method is in principle the same as dual fuel engine, but regarding engine structure, there are two independent speed regulators of diesel fuel and biogas fuel [11,20,36]. With this structure, the engine can reuse diesel when necessary. This option is suitable for places with limited biogas supply.

Research and design for conversion of an original marine diesel engine into a mixed fuel (biogas-diesel) engine. In which the post-conversion engine can run with biogas in the form of mixed fuel, diesel fuel plays an ignition role for the biogas/air mixture; or can operate with diesel fuel as the original engine.

2. MATERIALS AND METHODS

2.1 Properties and requirements of biogas

Biogas is the product of anaerobic decomposition of organic compounds [16]. The composition of biogas is mainly CH₄, CO₂ and other components such as N₂, H₂S, O₂, CO, ... Methane is used as fuel that is the main component of biogas, and other components do not play a role in heat generation during combustion of biogas.

Table 1: Components in biogas [26]

Compounds	Symbol	% Volume
Methane	CH ₄	50-75
Carbonic	CO ₂	25-45
Steam	H ₂ O	2 (20°C) – 7 (40°C)
Oxygen	O ₂	<2
Nitrogen	N ₂	<2
Ammonia	NH ₃	<1
Hydro	H ₂	<1
Hydrosulfite	H ₂ S	<1

Table 2. The concentration of CH₄ (theoretical) [28]

Material	Liter gas/kgNL	CH ₄ [%]	CO ₂ [%]
Protein	700	70÷71	29÷30
Fat	1.200-1.250	67÷68	32÷33
Carbohydrates	790-800	50	50

Table 3. shows physical properties of biogas.

Table 3: Physical properties of biogas [25]

Properties	CH ₄	CO ₂
Molecular weight	16,04	44,01
Proportion	0,554	1,52
Boiling point	144°C	60°C
Freezing point	-165°C	-39°C
Density	0,66 kg/m ³	1,82 kg/m ³
Dangerous temperature	64,5°C	48,9°C
Dangerous pressure	45,8 KG/cm ²	73 KG/cm ²
Specific heat capacity (1KG / cm ²)	6,962.10 ⁻⁴ J/kg ⁰ C	
Rate Cv /Cp	1,037	1,303
Burning heat	55,403 J/kg	
The rate of fire completely in the air	0,0581 (mass)	

The content of methane in the composition of biogas is used to determine the heating value of biogas. The formula for determining the heating value of biogas is:

$$Q_{\text{biogas}} = Q_{\text{CH}_4} \times \% \text{CH}_4 \quad (1)$$

In which: Q_{biogas} is the heating value of biogas, Q_{CH_4} is the heating value of methane, % CH₄ is the content by volume of CH₄.

The criteria for determining the standard for biogas are Heating Value - HV, Specific Gravity - SG, Wobbe Index, Methane Number.

Depending on the heating value is burning high heating value (HHV) or lower heating value (LHV) that have low or high Wobbe index. The Wobbe WI criteria are defined in the European gas fuel standards table (Table 4). According to European regulations, there are two groups of gas fuels: the group with high heating value (H group) and the group with low heating value (L group). H Group is for gas containing a large amount of methane and some other hydrocarbons. The L group for gases containing less methane and contains a significant amount of carbon dioxide or nitrogen.

Table 4: The criteria follow the DVGW G 260 standard set [37]

Criteria	Symbol	Unit	L group	H group	Note
Standard density	d		0,55 – 0,7		Allow deviation
Heating value	HV	KWh/m ³	8,4 – 13,1		Allow deviation
Wobbe index	WI	kWh/m ³	10,5 – 13,0	12,8– 15,7	Strict rules

Sweden has a set of national standards for biogas as fuel for transport vehicles in 1999. Tables 5 and 6 describe the main parameters of the standard.

Table 5: Swedish biogas standard [38]

Criteria	Unit	Limitation in regulations
Low Wobbe index	kWh/m ³	12,2 – 13,2 ([CH ₄] = 95-99%)
MON	-	>130
Dew point of water	°C	<t _{ambient} -5
CO ₂ + O ₂ + N ₂	% vol	<5
O ₂	% vol	<1
Total sulfur	mg/m ³	<23
NH ₃	mg/m ³	20

Table 6: German biogas standard

Criteria	Unit	Limitation in regulations
High Wobbe index	kWh/m ³	10,5-13 (in H) 12,8-15,7 (in H)
Standard density	-	0,55-0,75
Dew point of water	°C	<nhiệt độ mặt đất
CO ₂	% vol	<6
O ₂	% vol	<3

2.2 Conversion engine

Diesel engine for generator K657 M2 6412 / 14 (Figure 1) was selected to study the conversion to use fuel including both biogas and diesel. The basic

parameters of the engine are shown in Table 7. The components of the engine's fuel system are shown in Figure 2.

Table 7: Marine diesel engine K657 M2 6412/14

Parameters	Value
Type	4 stroke, no turbochargers
Number of cylinder	i = 6
Bore	D = 120 mm
Stroke	S = 140 mm
Rated rotation	n = 1500 v/ph
Rated power	Ne = 50 kW
Fuel consumption rate	g _e = 264 g/kW.h
Crank radius	Rc = 70 mm
Length of connection rod	l = 252 mm
Compression ratio	ε = 15

**Figure 1:** Marine diesel engine K657 M2 6412/14

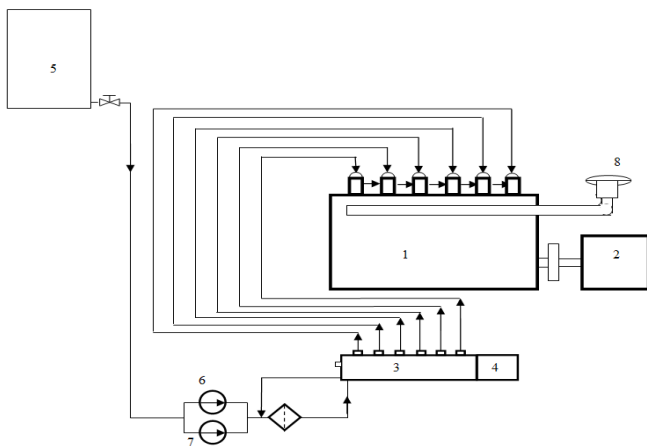


Figure 2: DO fuel system of marine diesel generator

1. Diesel engine; 2. Generator; 3. High-pressure pump; 4. Governor; 5. DO service tank; 6. Boost pump; 7. Hand pump; 8. Air filter.

The original engine uses diesel fuel (DO), has a fuel system diagram as shown in Figure 2. The engine uses a high-pressure cluster pump (Figure 3) in combination with a mechanical speed regulator.

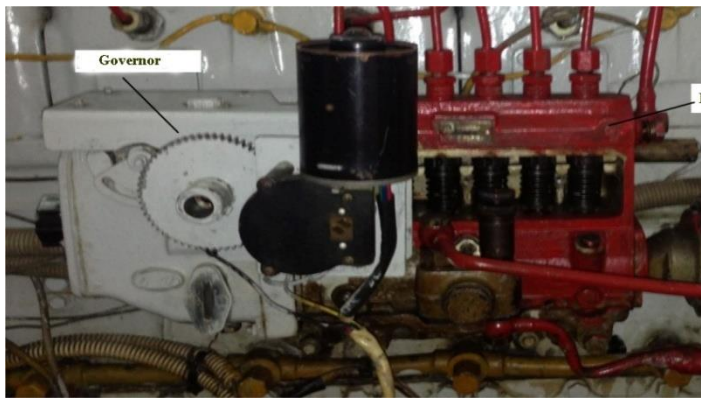


Figure 3: High-pressure pump

3. CALCULATION OF BIOGAS FUEL SUPPLY SYSTEM FOR ENGINES

3.1 Biogas fuel supply system

3.2

When using biogas fuel diagram of the fuel supply system for a diesel engine for generator K657 M2 6412 / 14 as shown in Figure 4.

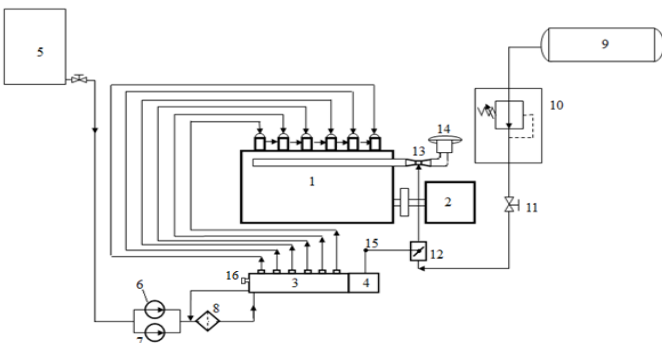


Figure 4: Biogas supply system of a marine diesel engine

1. Diesel engine; 2. Generator; 3. High-pressure pump; 4. Governor; 5. DO service tank; 6. Boost pump; 7. Hand pump; 8. Fuel filter; 9. Biogas tank; 10. Regulator; 11. Biogas cut down valve; 12. Biogas supply valve; 13. Mixer; 14. Air filter; 15. Control unit for the mixer; 16. Gear of high-pressure pump.

3.2 Calculate the mixer

Calculate the mixer to determine the following sizes: mixer size; throat mixing size; the size of a biogas digester.

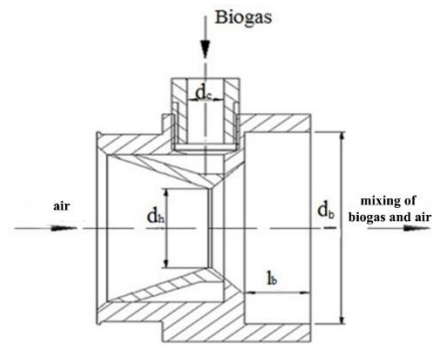


Figure 5: Diagram of calculating sizes

3.3 Determine the flow of diesel fuel and biogas when the engine uses mixed fuel

The low heating value of biogas is calculated according to Mendeleev formula:

$$Q_H = 0,385 \cdot CH_4 \cdot 1000 \quad [\text{kJ}/\text{m}^3] \quad (1)$$

The low heating value of biogas is:

$$Q_{HB} = \frac{Q_H}{\rho_B} \quad [\text{kJ}/\text{kg}] \quad (2)$$

To achieve a power of 50 kW, the heat generated by burning diesel fuel is complete:

$$Q_0 = \frac{Q_{HD} \cdot G_{nl}}{3,6} \quad [\text{J}/\text{s}] \quad (3)$$

In which: Q_{HD} is the low heating value of diesel fuel, $Q_{HD} = 42530$ (kJ/kg) G_{nl} of diesel fuel consumed in 1 hour,

$$G_{nl} = \frac{N_e \cdot g_e}{1000} \quad [\text{kg}/\text{h}] \quad (4)$$

When switching to using diesel/biogas mixture, the amount of fuel supplied to the engine to ensure the operation of the engine in idle mode and provide enough energy to ensure the combustion process of biogas/air. Assuming that when the engine runs in full-load mode, the amount of heat emitted by diesel fuel is 5%, and this amount is adjusted constantly throughout the engine's working process.

The heat generated by diesel fuel when the engine works:

$$Q_{0D} = \frac{Q_0 \cdot 0,5}{100} \quad [\text{J}/\text{s}] \quad (5)$$

The heat generated by biogas fuel is:

$$Q_{0B} = Q_0 - Q_{0D} \quad [\text{J}/\text{s}] \quad (6)$$

The amount of biogas needed to supply the engine in 1 hour will be:

$$G_{nIB} = \frac{Q_{0B} \cdot 3,6}{Q_{HB}} \quad [\text{kg}/\text{h}] \quad (7)$$

The amount of diesel fuel supplied to the engine in 1 hour is:

$$G_{nLD} = \frac{Q_{0D} \cdot 3,6}{Q_{HD}} \quad [\text{kg/h}] \quad (8)$$

The total amount of fuel for biogas and diesel for 1 hour is:

$$G_{nl} = G_{nLD} + G_{nLB} \quad [\text{kg/h}] \quad (9)$$

The mass fraction of diesel fuel in 1 kg mixed is:

$$D_{hh} = \frac{G_{nLD}}{G_{nl}} \cdot 100\% \quad (10)$$

The mass fraction of biogas in 1 kg mixed is:

$$B_{hh} = \frac{G_{nLB}}{G_{nl}} \cdot 100\% \quad (11)$$

Heating value of diesel / biogas mixture is:

$$Q_H = Q_{HD} \cdot D_{hh} + Q_{HB} \cdot B_{hh} \quad [\text{kJ/kg}] \quad (12)$$

Calculation results are:

G_{nLB} (kg/h)	G_{nLD} (kg/h)	G_{nl} (kg/h)	Q_H (kJ/kg)
19,08	0,657	19,737	28330

3.4 Calculate the mixing chamber diameter

The formula for determining the composite chamber diameter is:

$$d_b = a_n \cdot \sqrt{V_h \cdot i \cdot \frac{n}{1000}} \quad [\text{mm}] \quad (13)$$

In which: d_b is the inner diameter of the mixing chamber (mm); V_h is the working volume of a cylinder, [dm³]; i is the number of cylinders that share a mixer; n is the speed of rotation of the engine [v / p]; a_n is the coefficient of oscillation of the gas flow, depending on the number of cylinders that share a mixer;

Table 8: The coefficient of variation of the gas flow

Number of cylinders	1	2	3	4	5	6
Coefficient a_n	24,2	17,1	14,15	13	12,85	11,9

- The length of the mixing chamber is determined as follows:

$$l_b = (0,8 \div 1,8) d_b \quad [\text{mm}] \quad (14)$$

With the above parameters, we have the following calculation results:

d_b (mm)	l_b (mm)
54	45

3.5 Calculate diffuse throat diameter

Choose a preliminary throat diameter:

$$d_h = (0,6 \div 0,8) d_b \quad [\text{mm}] \quad (15)$$

The vacuum at the throat diffuses Δp_h :

$$\Delta p_h = \frac{\rho_{kk}}{2} \left[S \cdot \left(\frac{D}{d_h} \right)^2 \cdot \frac{n \cdot i}{2 \cdot 60} \cdot \frac{\eta_n}{\mu_h} \right]^2 \quad [\text{N/m}^2] \quad (16)$$

In which: S is piston stroke, [mm]; D is the cylinder diameter, [mm]; n is engine speed, [rpm]; d_h is diffuse throat diameter, [mm]; μ_h is the flow coefficient of the throat ($\mu_h = 0,8 - 0,9$); η_n is the gas loading coefficient.

The speed of air flow through the diffuser throat W_{kk} is calculated as follows:

$$W_{kk} = \sqrt{\frac{2 \Delta p_h}{\rho_{kk}}} \quad [\text{m/s}] \quad (17)$$

In which: ρ_{kk} is the density of air, (kg/m³); Δp_h is diffuse throat vacuum, (N/m²)

Determine the exact diameter of the throat:

$$G_{kk} = \mu_h \cdot f_h \cdot W_{kk} \cdot \rho_{kk} = \mu_h \cdot \frac{\pi \cdot d_h^2}{4} \cdot W_{kk} \cdot \rho_{kk} \quad [\text{m}^3/\text{h}] \quad (18)$$

In which: G_{kk} air flow through the diffusion throat, can be determined

$$G_{kk} = \eta_v \cdot V_h \cdot \frac{n \cdot i}{120} \cdot \rho_{kk} \quad (19)$$

So we have a diffuse throat diameter that is defined as follows:

$$d_h = \sqrt{\frac{4 G_{kk}}{\mu_h \cdot \pi \cdot W_{kk} \cdot \rho_{kk}}} \quad (20)$$

With the basic parameters: ε is the compression ratio of the engine, $\varepsilon = 15$; γ_r is the residual gas coefficient, $\gamma_r = 0,005$; T_0, P_0 are temperature and air pressure, $T_0 = 293$ [K] and $P_0 = 1$ [kG/cm²]; T_a, P_a is the temperature and pressure in the cylinder at the end of the charging process, $P_a = 0,9 \cdot P_0 = 0,9$ [kG / cm²] and $T_r = 700$ [K] is the gas temperature.

Results calculated:

Δp_h (N/m ²)	W_{kk} (m/s)	G_{kk} (kg/s)	d_h (mm)
9169	126	0.1256	36

Therefore, we choose the diameter throat $d_h = 36$ [mm].

3.6 Calculate the diameter of the biogas supply

The expression determines the speed of biogas flow through the feed pipe:

$$W_b = \sqrt{\frac{2 \Delta p_h}{\rho_b}} \quad [\text{m/s}] \quad (21)$$

In which: Δp_h is diffuse throat vacuum, Δp_h [N / m²]; ρ_b is the density of biogas, $\rho_b =$ [kg / m³];

Diameter of biogas supply hole will be:

$$F_{vp} = \frac{G_{nLB}}{W_b \cdot \rho_b} \quad [\text{m}^2] \quad (22)$$

$$d_{vp} = \sqrt{\frac{4 \cdot F_{vp}}{\pi}} \quad [\text{mm}] \quad (23)$$

The calculated result is:

W_b (m/s)	F_{vp} (m ²)	d_{vp} (mm)
142,7	$4,126 \cdot 10^{-5}$	7,25

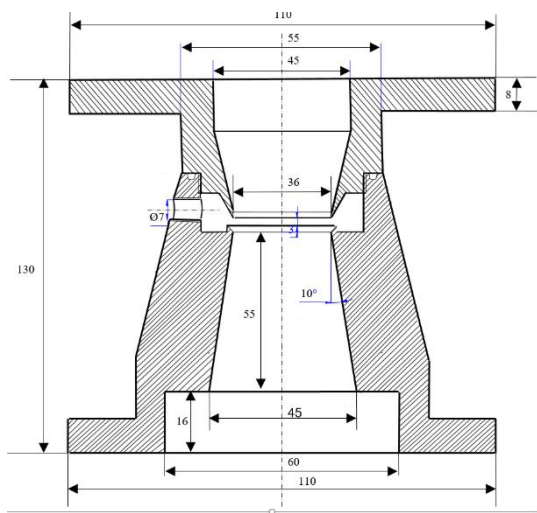


Figure 6: The structure of mixer with a donuts-shaped throat

For convenience of processing, select:

- Mixing chamber diameter: $d_b = 45$ [mm];
- Mixing chamber length: $l_b = 55$ [mm];
- Diffuse throat diameter: $d_h = 36$ [mm];
- Biogas supply hole diameter: $d_{vp} = 7$ [mm].

4. CONCLUSION

Based on the study of calculation of biogas fuel supply system for K657 M2 6412 / 14 engine can give some conclusions:

A method to convert small-sized diesel engine hybrid generators to the biogas and diesel mixture has been found.

Calculated devices for biogas fuel supply system applied to a specific engine.

The conversion of diesel engines to the use of mixed fuels biogas and diesel does not significantly change the structure of the original engine, so the cost of equipment for biogas fuel supply and engine conversion is not large. , the major conversion is to change the fuel supply system, speed regulator and air intake system.

However, the use of biogas fuel for ship engines will encounter some problems such as onboard storage problems, strict requirements of safety for ships and the current supply is not yet popular.

Since the topic is currently in the scope of theoretical research, it is not possible to fully appreciate all the features of biogas use for marine diesel engines.

REFERENCES

- [1] Fan, J., Wang, D., Kang, L. 2018. Development of renewable biomass energy by catalytic gasification: Syngas production for environmental management. *Energy Sources, Part A Recover. Util. Environ. Eff.*, 40 (24), pp. 2941–2947.
- [2] Hoang, A.T. 2018. Waste heat recovery from diesel engines based on Organic Rankine Cycle. *Applied Energy*, 231, pp. 138–166.
- [3] Patel, N.K., Kapadia, R.G., Gandhi, R.Y., Shah, S.N. 2017. Engine performance, emission and fluorescence study of fuel from plant oils. *Journal of Mechanical Engineering Research and Developments*, 40 (4), pp. 673–691.
- [4] Rosen, M.A. 2018. Environmental sustainability tools in the biofuel industry. *Biofuel Research Journal*, 5 (1), pp. 751–752.
- [5] Hoang, A.T., Pham, V.V. 2018. A review on fuels used for marine diesel engines. *Journal of Mechanical Engineering Research and Developments*, 41 (4), pp. 22–32.
- [6] Hoang, A.T. 2018. A report of the oil spill recovery and treatment technologies to reduce the marine environment pollution. *Int. J. e-Navigation Marit. Econ.*, 9, pp. 35–49.
- [7] Christiansen, K., Raman, D.R., Hu, G., Anex, R. 2018. First-order estimates of the costs, input-output energy analysis, and energy returns on investment of conventional and emerging biofuels feedstocks. *Biofuel Research Journal*, 5 (4), pp. 894–899.
- [8] Kumar, M.V., Babu, A.V., Kumar, P.R., Reddy, S.S. 2018. Experimental investigation of the combustion characteristics of Mahua oil biodiesel-diesel blend using a DI diesel engine modified with EGR and nozzle hole orifice diameter. *Biofuel Research Journal*, 5 (3), pp. 863–871.
- [9] Hoang, A.T., Pham, V.V. 2019. Impact of jatropha oil on engine performance, emission characteristics, deposit formation, and lubricating oil degradation. *Combustion Science and Technology*, pp. 1–16.
- [10] Hoang, A.T., Le, A.T. 2019. A review on deposit formation in the injector of diesel engines running on biodiesel. *Energy Sources, Part A Recover. Util. Environ. Eff.*, 41 (5), pp. 584–599.
- [11] Imran, A., Bramer, E.A., Seshan, K., Brem, G. 2018. An overview of catalysts in biomass pyrolysis for production of biofuels. *Biofuel Research Journal*, 5 (4), pp. 872–885.
- [12] Yang, W., Casey, J.F., Gao, Y., Li, J. 2019. A new method of geochemical allocation and monitoring of commingled crude oil production using trace and ultra-trace multi-element analyses. *Fuel*, 241, pp. 347–359.
- [13] Tuan, H.A., Quang, C.M. 2018. A mini review of using oleophilic skimmers for oil spill recovery. *Journal of Mechanical Engineering Research and Developments*, 41 (2), pp. 92–96.
- [14] Demirbaş, A. 2006. Global Renewable Energy Resources. *Energy Sources, Part A Recover. Util. Environ. Eff.*, 28 (8), pp. 779–792.
- [15] Hoang, A.T., Nguyen, D.C. 2018. Properties of DMF-fossil gasoline RON95 blends in the consideration as the alternative fuel. *Int. J. Adv. Sci. Eng. Inf. Technol.*, 8 (6).
- [16] Gnanamoorthi, V., Mohandoss, N.M. 2018. Combustion, performance and emission analysis of dual fuel engine using tsrb biogas. *Energy Sources, Part A Recover. Util. Environ. Eff.*, pp. 1–13.
- [17] Hoang, A.T., Bui, X.L., Pham, X.D. 2018. A novel investigation of oil and heavy metal adsorption capacity from as-fabricated adsorbent based on agricultural by-product and porous polymer. *Energy Sources, Part A Recover. Util. Environ. Eff.*, 40 (8), pp. 929–939.
- [18] Mofijur, M., Rasul, M.G., Hyde, J., Azad, A.K., Mamat, R., Bhuiya, M.M.K. 2016. Role of biofuel and their binary (diesel–biodiesel) and ternary (ethanol–biodiesel–diesel) blends on internal combustion engines emission reduction. *Renewable & Sustainable Energy Reviews*, 53, pp. 265–278.
- [19] Si, T., Cheng, J., Zhou, F., Zhou, J., Cen, K. 2017. Control of pollutants in the combustion of biomass pellets prepared with coal tar residue as a binder. *Fuel*, 208, pp. 439–446.
- [20] Karthikeyan, S., Prathima, A. 2016. Engine emission characteristics of algal biofuel with micro emulsion. *Energy Sources, Part A Recover. Util. Environ. Eff.*, 38 (24), pp. 3661–3667.
- [21] Hoang, A.T., Tran, Q.V., Al-Tawaha, A.R.M.S., Pham, V.V., Nguyen, X.P. 2019. Comparative analysis on performance and emission characteristics of an in-Vietnam popular 4-stroke motorcycle engine running on biogasoline and mineral gasoline. *Renew. Energy Focus*, 28, pp. 47–55.
- [22] Hoang, A.T., Pham, V.V. 2019. A study of emission characteristic, deposits, and lubrication oil degradation of a diesel engine running on preheated vegetable oil and diesel oil. *Energy Sources, Part A Recover. Util. Environ. Eff.*, 41 (5), pp. 611–625.
- [23] Abdoulmoumine, N., Adhikari, S., Kulkarni, A., Chattanathan, S. 2015. A review on biomass gasification syngas cleanup. *Applied Energy*, 155, pp. 294–307.

- [24] Nizami, A.S., Rehan, M. 2018. Towards nanotechnology-based biofuel industry. *Biofuel Res. J.*, 5 (2), pp. 798-799.
- [25] Khoshnevisan, B., Tsapekos, P., Alfaro, N., Díaz, I., Fdz-Polanco, M., Rafiee, S., Angelidaki, I. 2017. A review on prospects and challenges of biological H₂S removal from biogas with focus on biotrickling filtration and microaerobic desulfurization. *Biofuel Research Journal*, 4 (4), pp. 741-750.
- [26] Quintino, F.M., Trindade, T.P., Fernandes, E.C. 2018. Biogas combustion: Chemiluminescence fingerprint. *Fuel*, 231, pp. 328-340.
- [27] Hoang, A.T. 2018. Prediction of the density and viscosity of biodiesel and the influence of biodiesel properties on a diesel engine fuel supply system. *Journal of Marine Science and Technology*, pp. 1-13.
- [28] Rahman, K.A., Ramesh, A. 2019. Studies on the effects of methane fraction and injection strategies in a biogas diesel common rail dual fuel engine. *Fuel*, 236, pp. 147-165.
- [29] Farzad, S., Mandegari, M.A., Görgens, J.F. 2016. A critical review on biomass gasification, co-gasification, and their environmental assessments. *Biofuel Research Journal*, 3 (4), pp. 483-495.
- [30] Náthia-Neves, G., de A. Neves, T., Berni, M., Dragone, G., Mussatto, S.I., Forster-Carneiro, T. 2018. Start-up phase of a two-stage anaerobic co-digestion process: hydrogen and methane production from food waste and vinasse from ethanol industry. *Biofuel Research Journal*, 5 (2), pp. 813-820.
- [31] Sivaraja, C.M., Sakthivel, G., Warke, V.R. 2018. Selection of optimum fuel blend to empower the energy efficiency in IC engine using decision system. *Energy Sources, Part A Recover. Util. Environ. Eff.*, 40 (6), pp. 693-708.
- [32] Pham, V.V. 2018. Analyzing the effect of heated wall surface temperatures on combustion chamber deposit formation. *Journal of Mechanical Engineering Research and Developments*, 41 (4), pp. 17-21.
- [33] Bateni, H., Saraeian, A., Able, C. 2017. A comprehensive review on biodiesel purification and upgrading. *Biofuel Research Journal*, 4 (3), pp. 668-690.
- [34] Hoang, A.T., Pham, M.T. 2018. Influences of heating temperatures on physical properties, spray characteristics of bio-oils and fuel supply system of a conventional diesel engine. *International Journal of Advanced Science, engineering and Technology*, 8 (5), pp. 2231-2240.
- [35] Hoang, A.T. 2019. Experimental study on spray and emission characteristics of a diesel engine fueled with preheated bio-oils and diesel fuel. *Energy*. <https://doi.org/10.1016/j.energy.2019.01.076>.
- [36] Kumar, S., Singh, A., Kumar, H. 2018. Assessment of tracing element characteristics of F-type fly and bottom ash mixture. *Energy Sources, Part A Recover. Util. Environ. Eff.*, 40 (24), pp. 2967-2973.
- [37] Miskolc, U.N.I. 2008. A register of all gas regulations and norms concerning the necessary gas quality for allowing the transport in the natural gas grid. *Europe*, 15 (8), pp. 1-64.
- [38] Gis, W., Jakóbiec, J., Żółtowski, A. 2012. Biogas as engine fuel. *Silniki spalinowe*, 51.

